### 3.4. Solved Problems - Clutch Drive System Design

## Problem 1

A plate clutch consists of a flat driven plate gripped between the driving plate and the pressure plate so that two active driving surfaces each having an inner diameter of $204 \mathbf{~ m m}$ and an outer diameter of 356 mm . The coefficient of friction is 0.4 . The working pressure is limited to $172 \mathrm{kN} / \mathrm{m}^{2}$.
(a) Assuming that the pressure is uniform, determine the power which can be transmitted at a rotational speed of $1000 \mathrm{rev} / \mathrm{min}$.
(b) If the clutch is worn so that the intensity of pressure is inversely proportional to the radius, the total axial force of the pressure plate remaining unaltered, calculate the power which can be transmitted at $1000 \mathrm{rev} / \mathrm{min}$, and the greatest intensity of pressure on the friction surfaces.

## Solution

(a) Uniform Pressure - Transmitted Power:

Data:

$$
\begin{aligned}
& \mathrm{p}=172 \mathrm{kNm}^{-2}=172 \times 10^{3} \mathrm{Nm}^{-2} \\
& \mathrm{r}_{1}=356 / 2 \mathrm{~mm}=0.178 \mathrm{~m} \\
& \mathrm{r}_{2}=204 / 2 \mathrm{~mm}=0.102 \mathrm{~m} \\
\therefore \quad & \mathrm{R}=140 \mathrm{~mm}=0.14 \mathrm{~m} \\
& \mathrm{n}=2
\end{aligned}
$$

Axial thrust force, $W=\pi \cdot p\left(r_{1}^{2}-r_{2}^{2}\right)=\pi x\left(172 \times 10^{3}\right)\left(0.178^{2}-0.102^{2}\right)=11.49 \mathrm{kN}$
Torque, $T=\frac{2}{3} \cdot \mu \cdot W \frac{\left(r_{1}^{3}-r_{2}^{3}\right)}{\left(r_{1}^{2}-r_{2}^{2}\right)} \times n=\frac{2}{3} \times 0.4 \times\left(11.49 \times 10^{3}\right) \frac{\left(0.178^{3}-0.102^{3}\right)}{\left(0.178^{2}-0.102^{2}\right)} \times 2=1318 \mathrm{Nm}$
Power, $\mathrm{P}=\mathrm{T} \omega=\frac{2 \pi N T}{60}=\frac{2 \pi \times 1000 \times 1318}{60}=\mathbf{1 3 8} \mathbf{k W}$
(b) Uniform Wear - Transmitted Power:

$$
\begin{aligned}
& \mathrm{T}=\mu \mathrm{WR} . \mathrm{n}=0.4\left(11.49 \times 10^{3}\right)(0.14) 2=1287 \mathrm{Nm} \\
& \text { Power, } \mathrm{P}=\mathrm{T} \omega=\frac{2 \pi N T}{60}=\frac{2 \pi \times 1000 \times 1287}{60}=\mathbf{1 3 5} \mathbf{k W}
\end{aligned}
$$

Axial thrust force, $W=2 \pi . c\left(r_{1}-r_{2}\right)=2 \pi . p . r\left(r_{1}-r_{2}\right)$ where p occurs at the smallest radius, i.e $\mathrm{r}_{2}$.

$$
\therefore \quad p=\frac{W}{2 \pi r_{2}\left(r_{1}-r_{2}\right)}=\frac{11.49 \times 10^{3}}{2 \pi \times 0.102(0.178-0.102)}=236 \mathbf{k N m}^{-2}
$$

## Problem 2

A multiple disc clutch consisting of 5 input discs and 4 output discs is shown in Figure 3.4. This clutch is required to transmit a maximum power of 2.7 kW at 1600 rpm , and the inner diameter of the clutch is restricted to 55 mm due to the size of the shaft. Making the assumption of:

## a. Uniform pressure

b. Uniform wear

Determine the required outside diameter of the discs and the required axial force. For both cases the coefficient of friction can be assumed to be 0.12, and the pressure is not to exceed $360 \mathrm{kNm}^{-2}$.

Solution
(a) Uniform Pressure - Outside Diameter and Required Axial Force:

Data:
$\mathrm{p}=360 \mathrm{kNm}^{-2}=360 \times 10^{3} \mathrm{Nm}^{-2}$
$\mathrm{r}_{1}=$ ?
$\mathrm{r}_{2}=55 / 2 \mathrm{~mm}=0.0275 \mathrm{~m}$
$\mu=0.12$
$\mathrm{n}=8$
$\mathrm{P}=2.7 \mathrm{~kW}=2.7 \times 10^{3} \mathrm{~W}$
$\mathrm{N}=1600 \mathrm{rpm}$
Total Torque, $T_{t}=\frac{60 \times P}{2 \pi N}=\frac{60 \times 2700}{2 \pi \times 1600}=16.11 \mathrm{Nm}$
Torque per pair of contact plates, $T=T_{t} / n=16.11 / 8=2.014 \mathrm{Nm}$

As torque, $T=\frac{2}{3} \cdot \pi \mu \cdot p\left(r_{1}^{3}-r_{2}^{3}\right) \mathrm{Nm}$

$$
\begin{aligned}
& \Rightarrow 2.014=\frac{2}{3} . \pi \times 0.12 \times 360 \times 10^{3}\left(r_{1}^{3}-(0.0275)^{3}\right) \\
& \Rightarrow r_{1}^{3}-(0.0275)^{3}=\frac{3}{2 \pi} \times \frac{2.014}{0.12 \times 360 \times 10^{3}} \\
& \Rightarrow r_{1}^{3}=\frac{3}{2 \pi} \times \frac{2.014}{0.12 \times 360 \times 10^{3}}+(0.0275)^{3} \\
\Rightarrow & \Rightarrow r_{1}^{3}=4.3060 \times 10^{-5} \\
& \Rightarrow r_{1}=0.0351 \mathrm{~m} \\
& =35.05 \mathrm{~mm} \\
& \Rightarrow d_{1}=70.1 \mathrm{~mm}
\end{aligned}
$$

Therefore, Axial thrust force, $W=\pi \cdot p\left(r_{1}^{2}-r_{2}^{2}\right)=\pi x\left(360 \times 10^{3}\right)\left(0.03505^{2}-0.0275^{2}\right)$

$$
=534.12 \mathrm{~N}
$$

(b) Uniform Wear - Outside Diameter and Required Axial Force

$$
\begin{aligned}
& \mathrm{T}=\mu \mathrm{WR} .=\mu \pi p\left(r_{1}^{2}-r_{2}^{2}\right)\left(\frac{r_{1}+r_{2}}{2}\right) \mathrm{Nm} \\
& \Rightarrow 2.014=0.12 \pi \times 360 \times 10^{3}\left(r_{1}^{2}-(0.0275)^{2}\right)\left(\frac{r_{1}+0.0275}{2}\right) \\
& \Rightarrow 2.014=135,716.80\left(r_{1}^{2}-(0.0275)^{2}\right)\left(\frac{r_{1}}{2}+0.01375\right) \\
& \Rightarrow 1.4840 \times 10^{-5}=\left(r_{1}^{2}-(0.0275)^{2}\right)\left(\frac{r_{1}}{2}+0.01375\right)
\end{aligned}
$$

This equation is difficult to solve, so the value is more easily obtained by assuming that $\mathrm{r}_{1}$ is equal to 35 mm , from part a), then equating the two sides of the equation:

$$
\begin{aligned}
\text { RHS } & =\left(r_{1}^{2}-(0.0275)^{2}\right)\left(\frac{r_{1}}{2}+0.01375\right) \\
& =\left(0.035-(0.0275)^{2}\right)\left(\frac{0.035}{2}+0.01375\right) \\
& =1.4648 \times 10^{-5}
\end{aligned}
$$

This is approximately equal to the LHS, but would ideally be within $1 \%$, so:

$$
\begin{aligned}
\% \text { diff } & =\frac{1.4840-1.4648}{1.4840} \times 100 \\
& =1.29 \%
\end{aligned}
$$

Therefore try $\mathrm{r}_{1}=35.1 \mathrm{~mm}$;

$$
\begin{aligned}
\text { RHS } & =\left(r_{1}^{2}-(0.0275)^{2}\right)\left(\frac{r_{1}}{2}+0.01375\right) \\
& =\left(0.0351-(0.0275)^{2}\right)\left(\frac{0.0351}{2}+0.01375\right) \\
& =1.4891 \times 10^{-5}
\end{aligned}
$$

This is approximately equal to the LHS, but would ideally be within $1 \%$, so:

$$
\begin{aligned}
\% \text { diff } & =\frac{1.4891-1.4840}{1.4840} \times 100 \\
& =0.35 \%
\end{aligned}
$$

Therefore $\mathrm{d}_{1}=70.2 \mathrm{~mm}$, not greatly different from part a).

Therefore, Axial thrust force, $W=\pi \cdot p\left(r_{1}^{2}-r_{2}^{2}\right)=\pi x\left(360 \times 10^{3}\right)\left(0.0351^{2}-0.0275^{2}\right)$

$$
=538.07 \mathrm{~N}
$$

## Problem 3

A cone clutch is designed to transmit 210 Nm of torque at 1220 rpm. The clutch contact surfaces have an outer diameter of 360 mm and the semi-cone angle is $6.5^{\circ}$. Assuming the face width is 70 mm and the coefficient of friction is 0.22 , determine the axial force required to transmit the torque assuming:
a. Uniform pressure
b. Uniform wear

## Solution

Data:
$\mathrm{T}=210 \mathrm{Nm}$
$\mathrm{D}_{1}=360 \mathrm{~mm}=0.36 \mathrm{~m}$
$\mathrm{r}_{1}=0.36 / 2 \mathrm{~m}=0.18 \mathrm{~m}$
$\beta=6.5^{0}$
$\mathrm{b}=70 \mathrm{~mm}$
$\mu=0.22$


From the geometry:
$r_{2}=r_{1}-x$
$\sin \beta=\frac{x}{b}$
$\Rightarrow x=b \sin \beta$
Substituting (2) into (1):
$\Rightarrow r_{2}=r_{1}-b \sin \beta$
$=0.18-0.07 \sin 6.5=0.1721 \mathrm{~m}$
a) Assuming uniform pressure:

$$
\begin{aligned}
& T=\frac{2}{3} \cdot \frac{\mu \cdot W}{\sin \beta} \frac{\left(r_{1}^{3}-r_{2}^{3}\right)}{\left(r_{1}^{2}-r_{2}^{2}\right)} \\
& \Rightarrow 210=\frac{2}{3} \cdot \frac{0.22 . W}{\sin 6.5} \frac{\left(0.18^{3}-0.1721^{3}\right)}{\left(0.18^{2}-0.1721^{2}\right)} \\
& \Rightarrow W=210 \times \frac{3}{2} \times \frac{\sin 6.5}{0.22} \times \frac{\left(0.18^{2}-0.1721^{2}\right)}{\left(0.18^{3}-0.1721^{3}\right)} \\
& \Rightarrow W=615.53 \mathrm{~N}
\end{aligned}
$$

b) Assuming uniform wear:

$$
\begin{aligned}
& T=\frac{\mu \cdot W R}{\sin \beta}=\frac{\mu \cdot W}{\sin \beta} \times \frac{r_{1}+r_{2}}{2} \\
& \Rightarrow 210=\frac{0.22 . W}{\sin 6.5} \times \frac{0.18+0.1721}{2} \\
& \Rightarrow W=\frac{210 \times 2 \sin 6.5}{0.22 \times(0.18+0.1721)} \\
& \Rightarrow W=613.79 \mathrm{~N}
\end{aligned}
$$

## Problem 4

A plate clutch has 5 driving discs and 4 driven discs, i.e. 8 pairs of contact surfaces, each of 185 mm external diameter and 135 mm internal diameter.
(a) Assuming uniform pressure, calculate the total axial spring load required to permit the clutch to transmit $38 \mathbf{k W}$ at $1470 \mathrm{rev} / \mathrm{min}$ if the coefficient of friction between the disc surfaces is 0.32.
(b) If there are 8 springs, each of stiffness $13 \mathbf{k N m}^{-1}$, and each of the contact surfaces has lost 0.145 mm due to wear, calculate the maximum power which can be transmitted under the above conditions:

## Solution

Data:
$\mathrm{P}=38 \mathrm{~kW}$
$\mathrm{N}=1470 \mathrm{rpm}$
$\mathrm{D}_{1}=185 \mathrm{~mm}=0.185 \mathrm{~m}$
$\mathrm{r}_{1}=0.185 / 2 \mathrm{~m}=0.0925 \mathrm{~m}$
$\mathrm{D}_{2}=135 \mathrm{~mm}=0.135 \mathrm{~m}$
$\mathrm{r}_{2}=0.135 / 2 \mathrm{~m}=0.0675 \mathrm{~m}$
$\mu=0.32$
$\mathrm{n}=8$
$\mathrm{k}=13 \mathrm{kNm}^{-1}=13 \times 10^{3} \mathrm{Nm}^{-1}$
Wear per contact surface $=0.145 \mathrm{~mm}$
(a) Total Torque, $T_{t}=\frac{60 \times P}{2 \pi N}=\frac{60 \times 38 \times 10^{3}}{2 \pi \times 1470}=246.85 \mathrm{Nm}$

Torque per pair of contact plates, $T=T_{t} / n=246.85 / 8=30.86 \mathrm{Nm}$
As torque, $T=\frac{2}{3} \cdot \mu \cdot W \frac{\left(r_{1}^{3}-r_{2}^{3}\right)}{\left(r_{1}^{2}-r_{2}^{2}\right)} \mathrm{Nm}$
$\Rightarrow 30.86=\frac{2}{3} .0 .32 . W \frac{\left(0.0925^{3}-0.0675^{3}\right)}{\left(0.0925^{2}-0.0675^{2}\right)}$
$\Rightarrow W=\frac{3}{2} \cdot \frac{1}{0.32} \cdot 30.86 \frac{\left(0.0925^{2}-0.0675^{2}\right)}{\left(0.0925^{3}-0.0675^{3}\right)}=1195.60 \mathrm{~N}$
(b) $\mathrm{W}_{\text {worn }}=\mathrm{W}-\mathrm{F}$, where $\mathrm{F}=\mathrm{k}_{\mathrm{T}} \cdot \mathrm{X}$
$\mathrm{k}_{\mathrm{T}}(8$ springs in parallel $)=8 \times 13 \times 10^{3}=104 \times 10^{3} \mathrm{Nm}^{-1}$
$\mathrm{x}(8$ contact pairs x two surfaces per pair x wear per contact surface $)=8 \times 2 \times 0.145 \mathrm{~mm}$

$$
=2.32 \mathrm{~mm}
$$

Therefore:

$$
\begin{aligned}
\mathrm{W}_{\text {worn }}= & 1195.60-104 \times 10^{3} \times 2.32 \times 10^{-3} \\
& =1195.60-241.28 \\
& =954.32 \mathrm{~N}
\end{aligned}
$$

Therefore:

$$
\begin{aligned}
T & =\mu W R x n \\
& =0.32 \times 954.32 \times \frac{(0.0925+0.0675)}{2} \times 8 \\
& =195.45 \mathrm{Nm}
\end{aligned}
$$

Therefore:

$$
\begin{aligned}
P & =T x \omega \\
& =195.45 \times \frac{2 \times \pi \times 1470}{60} \\
& =30,086.54 \mathrm{~W} \\
& =30.09 \mathrm{~kW}
\end{aligned}
$$

